



ACID GAS ENRICHMENT – NEW WRINKLES ON AN OLD PROCESS

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Agenda



- Introduction & Background
- Case Study Design Basis & Definition of Cases
- Process Comparison
- CapEx, OpEx & Lifecycle Cost Comparison
- Summary & Conclusions
- Next Steps

Introduction



Lean acid gas results in the following SRU complications

- Cool thermal reactor temperature and flame instability
- Poor destruction of impurities - hydrocarbon (BTX) and NH_3

FUEL GAS CO-FIRING

- ❌ Fuel consumption OpEx (RF, RGG, Incin.)
- ❌ Increases size of SRU/TGTU
- ❌ Possible catalyst damage – sooting/ O_2 fire

ACID GAS ENRICHMENT

- ❌ AGE amine circulation OpEx
- ❌ More equipment/operating complexity
- ✅ Reduces size of SRU/TGTU
- ✅ Improved acid gas quality
– higher $\text{H}_2\text{S}\%$ & reduced impurities

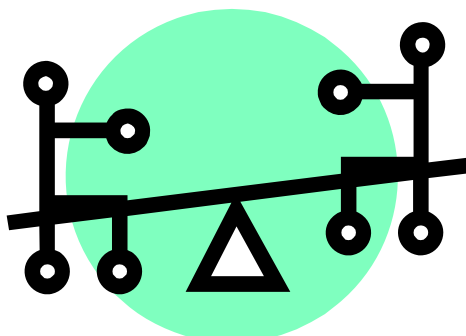


Process Parameters Impacting Selectivity



Selective

- Lower P
- Lower T
- Optimized circulation
- Minimal H_2S lean loading (if pinched)



Not Selective

- Higher P
- Higher T (μ)
- Over-circulated

Mass Transfer Rates Control Selectivity



- Pickup Rate $\propto k A (\Delta\text{Concentration})$

Mass Transfer
Coefficient



Area



Driving force



- Extent of **disequilibrium** (NOT at Equilibrium) drives mass transfer
- H₂S often gas film controlled
- CO₂ often liquid film controlled
- More area → More mass transfer
 - Good for H₂S, not so good for CO₂

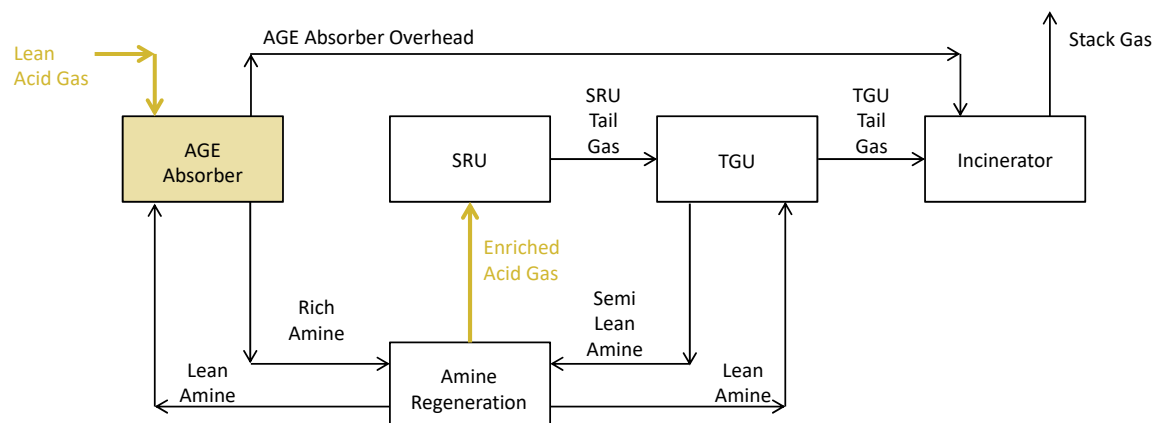
Mass Transfer Rate



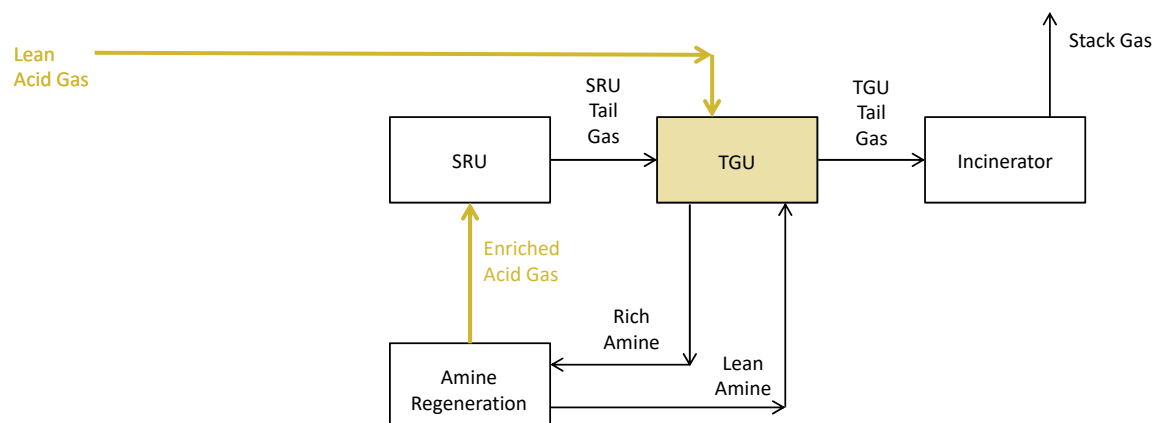
- Area & mass transfer coefficients depend on...
 - Gas & liquid loads (rates)
 - Mass transfer internals type
 - Hydraulics (specific tower internals)
 - Physical properties (density, viscosity, diffusion)
 - f (T, P, solvent concentration and type)
- ProTreat[®] software used for this study accounts for all these factors



Typical Acid Gas Enrichment BFD



The New Wrinkle...





Case Study Design Basis

ACID GAS FEED

Component	Mole %
Water	10.48
Hydrogen Sulfide	26.86
Carbon Dioxide	62.18
C1	0.27
C2	0.10
C3	0.07
C4	0.04
C5	0.01
Total Flow	4,838 kmol/h

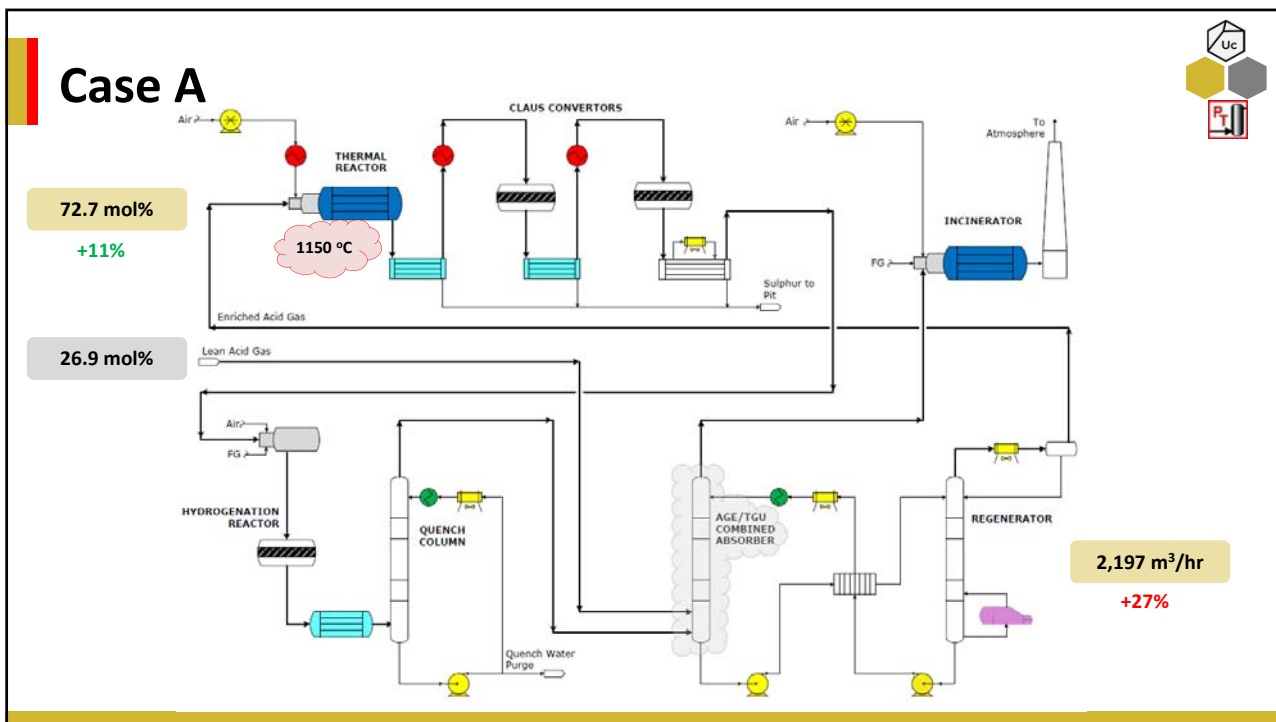
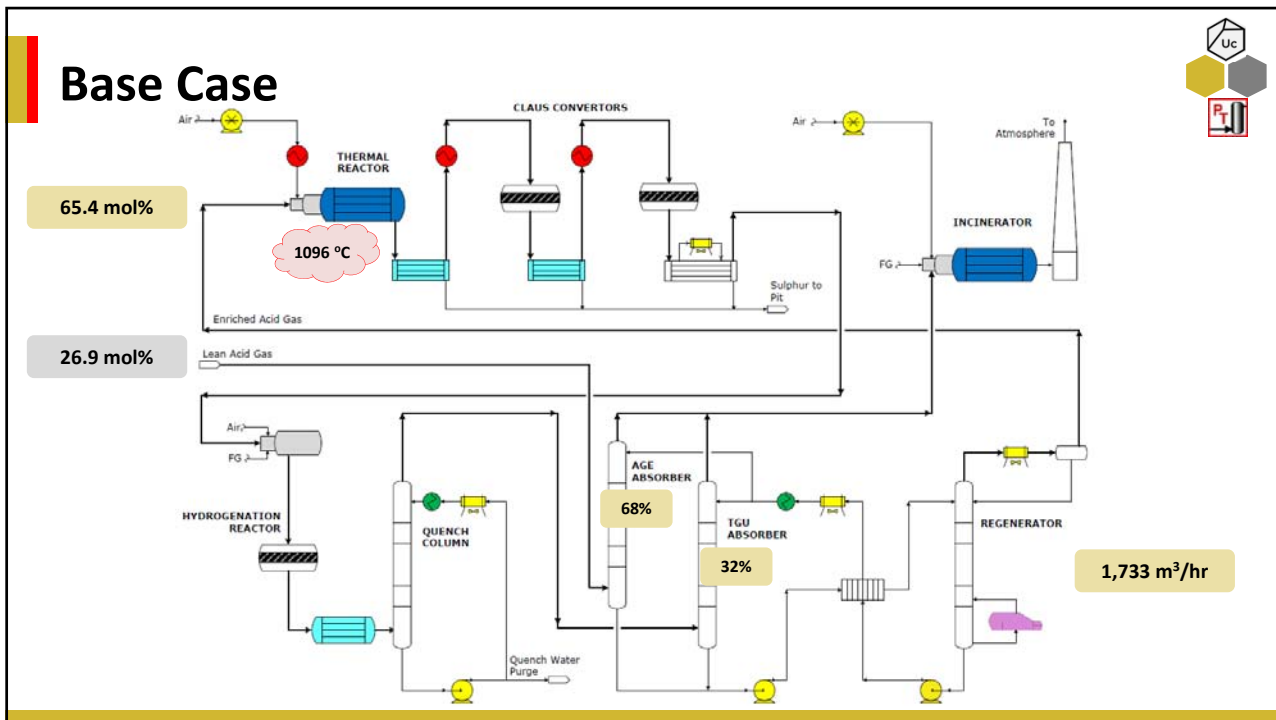
- 1,000 MTPD
- AG Pressure: ~0.9 barg
- AG Temperature: 60°C
- 40 wt% MDEA AGE/TGTU
- 99.9% SRE
- Air cooling to 60°C
- Propane trim cooling

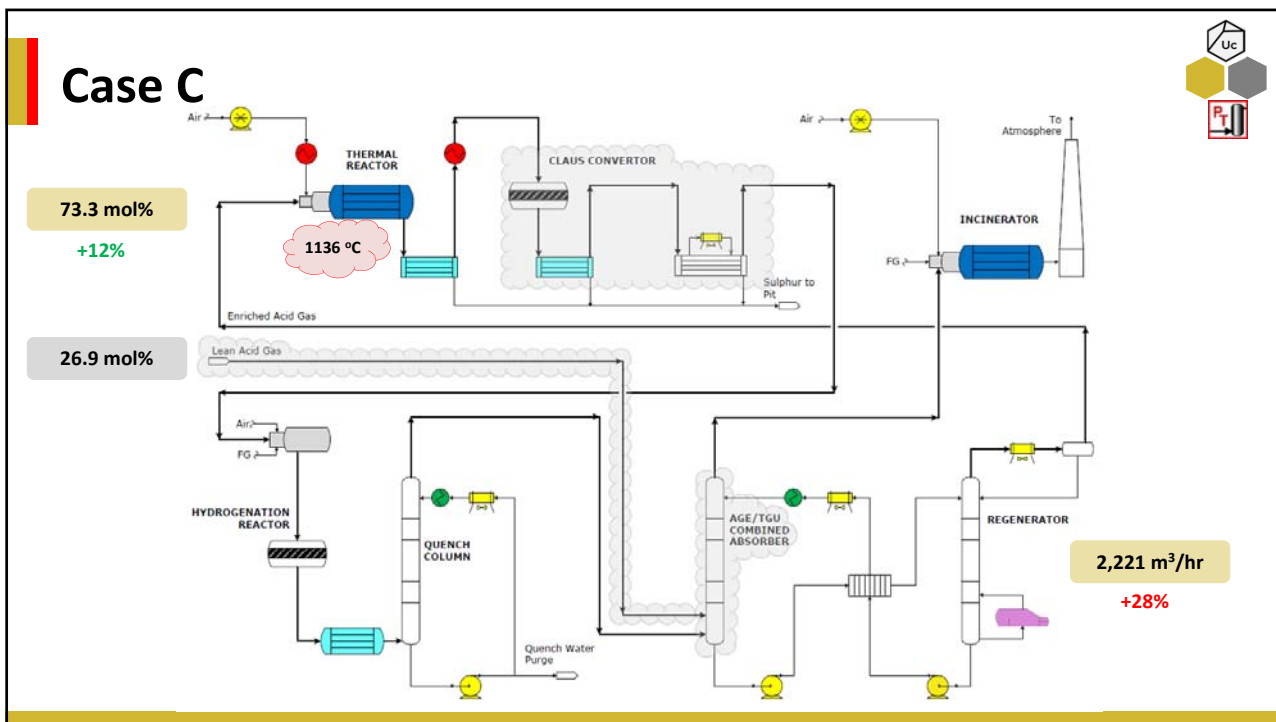
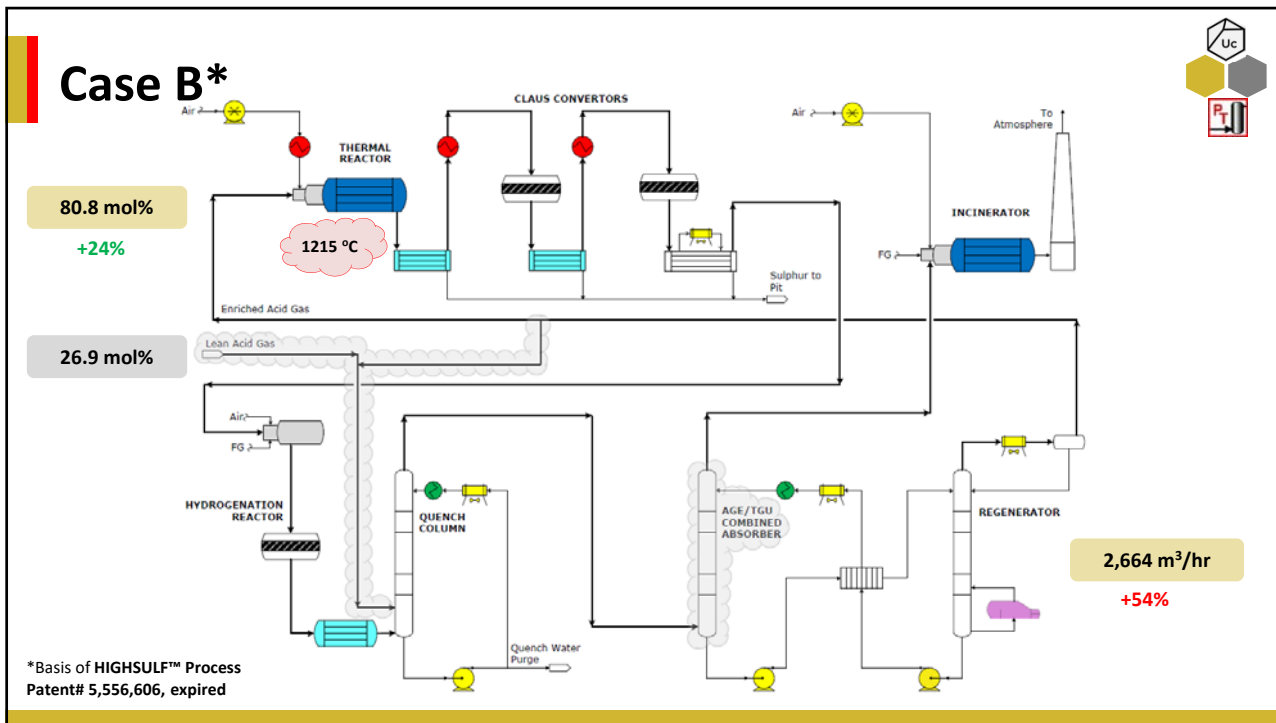
Cases

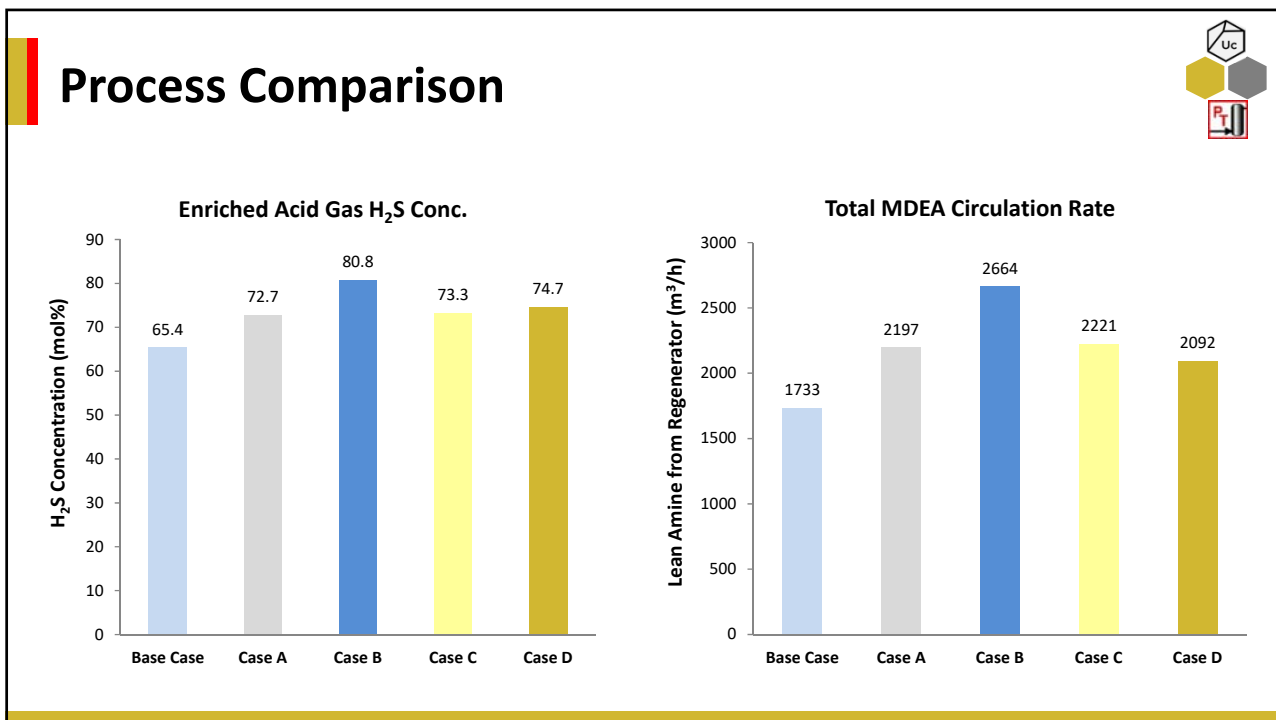
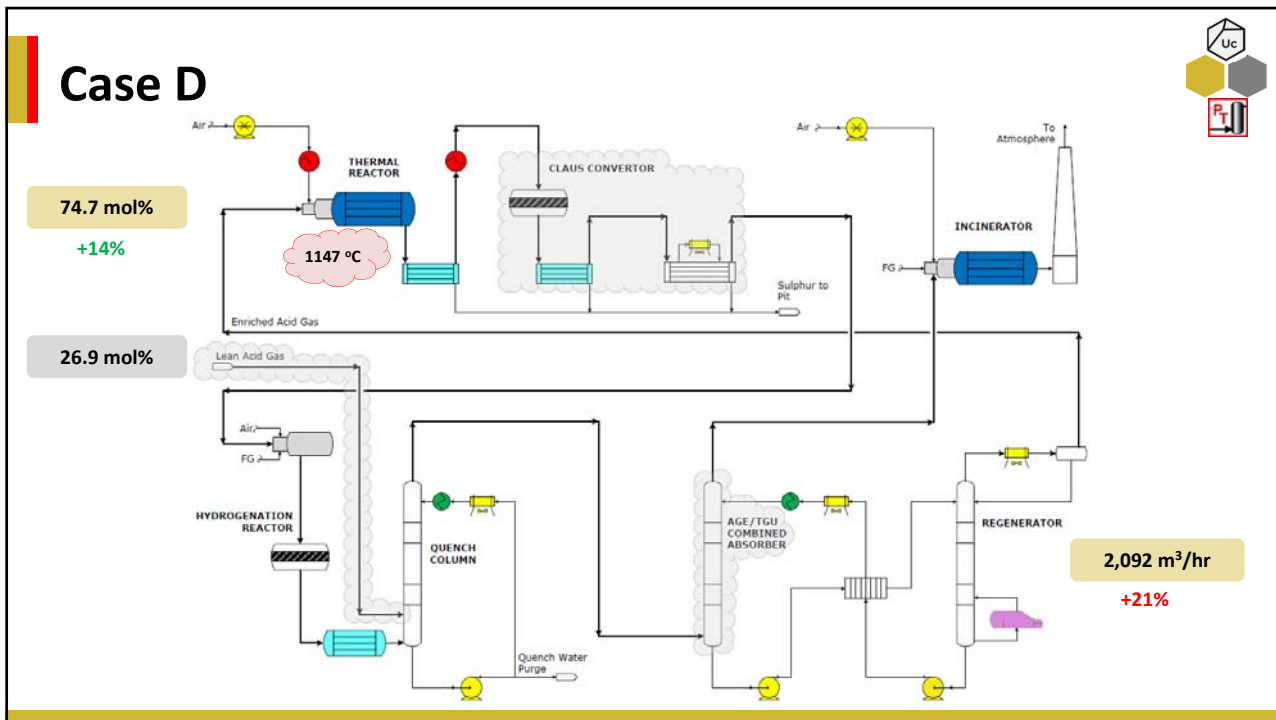


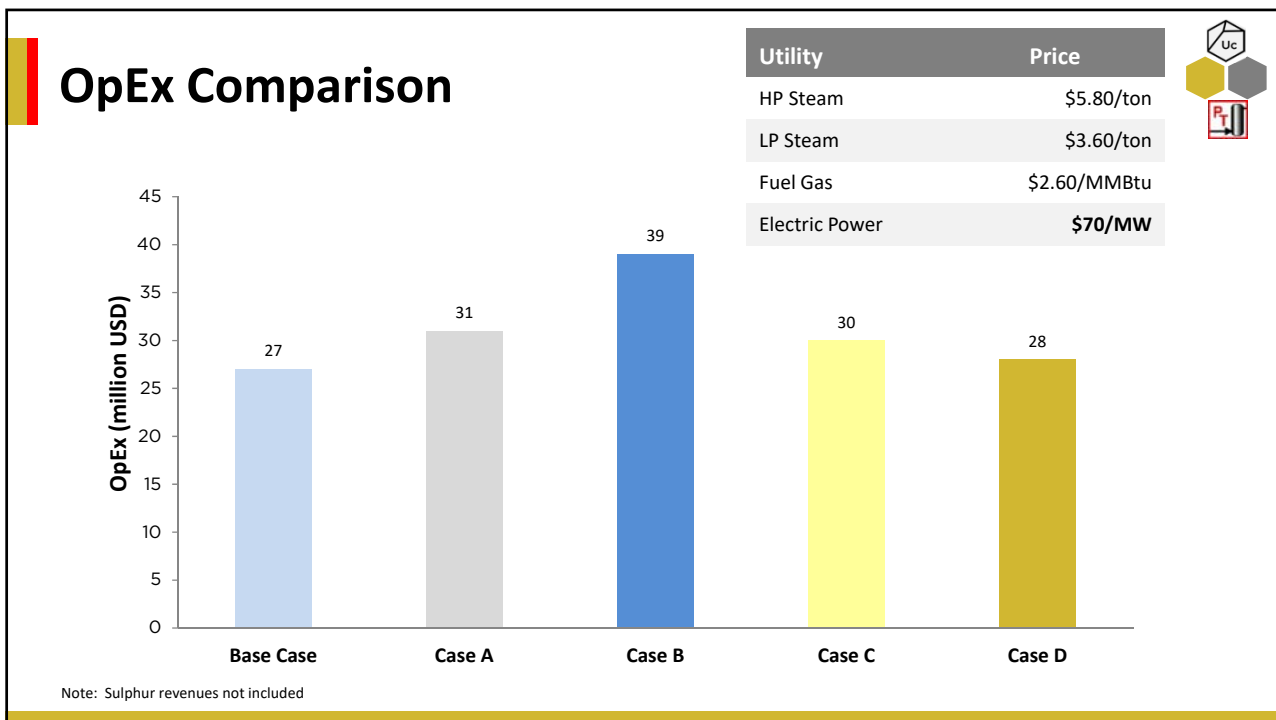
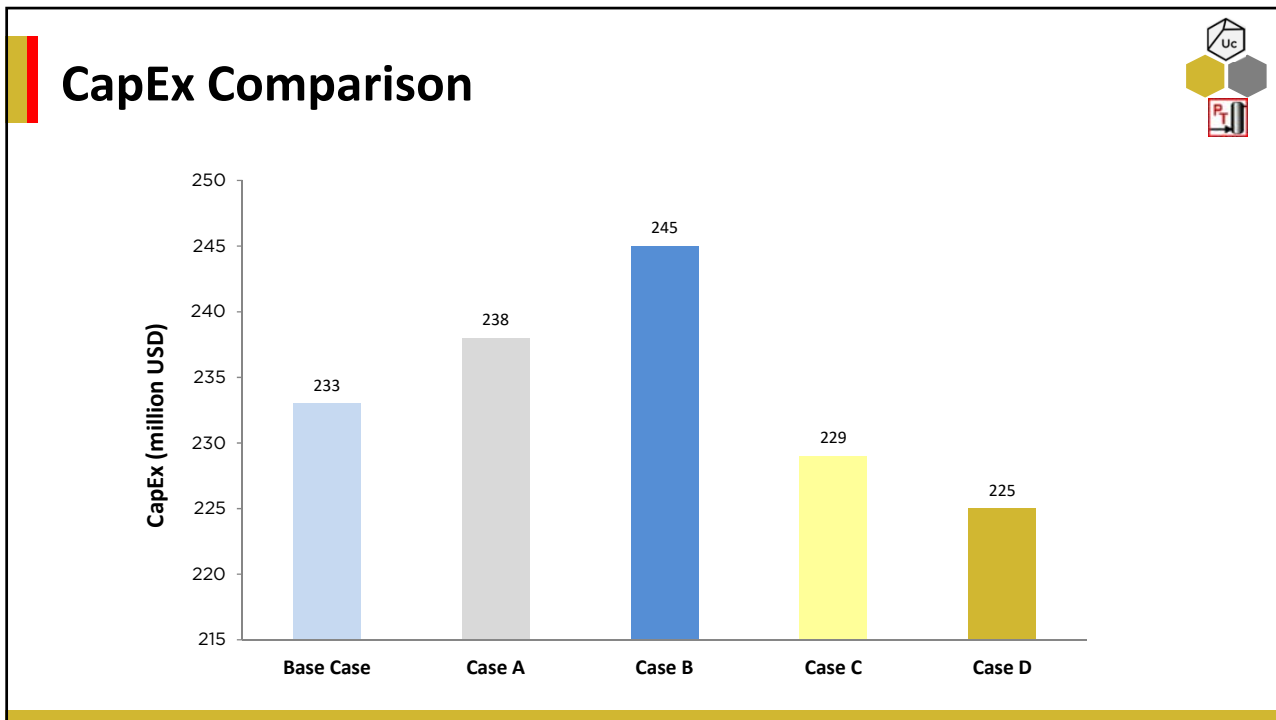
CASE	AGE ABSORBER	LEAN AG FEED TO:	ENRICHED AG FEED TO:	# OF CLAUS STAGES
Base	Standalone	AGE Absorber	SRU	2
A	Combined AGE/TGU	AGE/TGU Absorber	SRU	2
B*	Combined AGE/TGU	Quench Column	SRU + Quench	2
C	Combined AGE/TGU	AGE/TGU Absorber	SRU	1
D	Combined AGE/TGU	Quench Column	SRU	1

*Basis of HIGHSULF™ Process
Patent# 5,556,606, expired



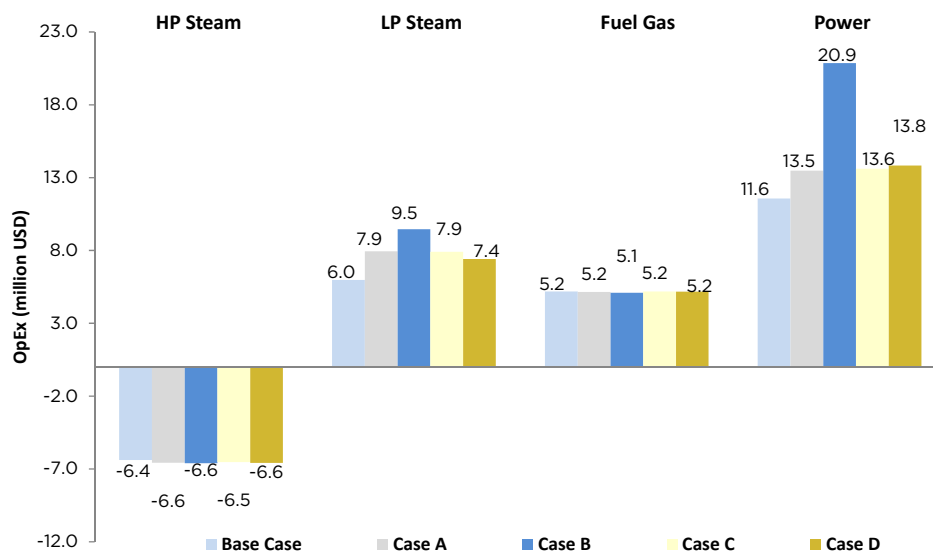




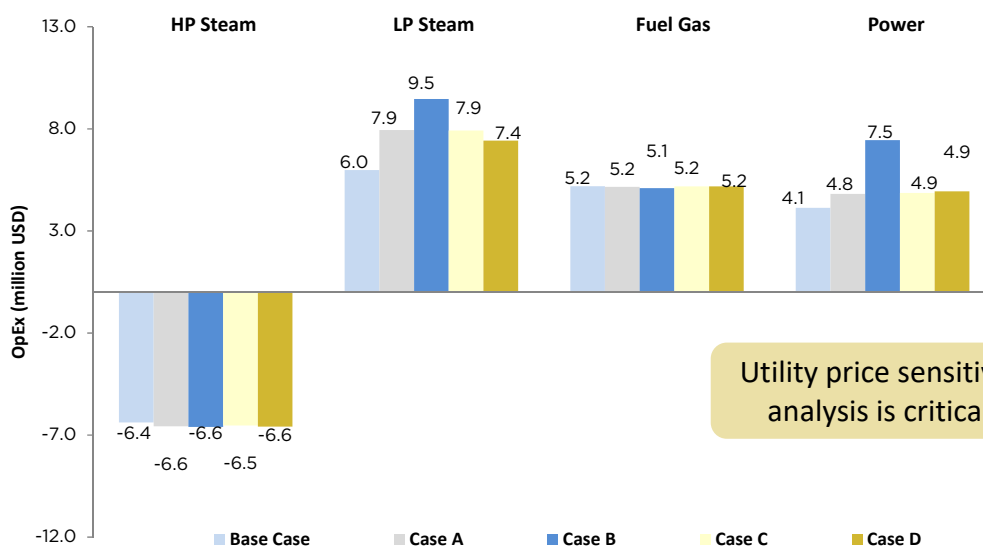




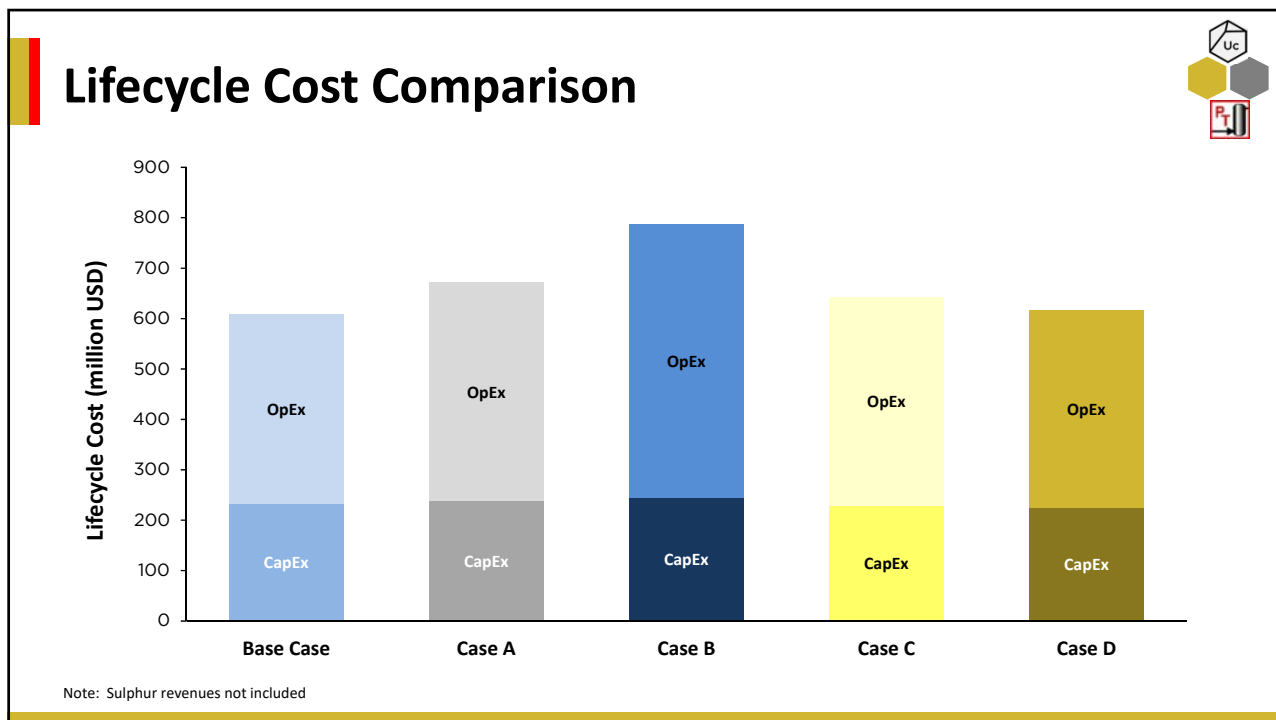
OpEx Comparison by Utility



Alternate OpEx Comparison by Utility (\$25/MW)



Utility price sensitivity analysis is critical!



Summary & Conclusions

- Acid gas enrichment improves acid gas quality & SRU operation
- Routing lean acid gas to **TGU absorber**
 - Improves enrichment
 - But increases CapEx & OpEx
- Routing lean acid gas to **quench column**
 - Improves enrichment even further
 - But also increases CapEx & OpEx further

Elimination of a Claus stage alleviates cost impact....
but may not be recommended (TGU bypass operation)

Next Steps



- Consider leaner acid gas to understand full range of benefits
- Other solvents?
- Off-ratio tail gas (H_2S rich) selectivity benefits (SINI HCR™)
- Compare AGE cases to fuel gas firing
- Assessment in cooler climate without refrigeration requirement
- **Utility price** sensitivity analysis
- Formal paper

